



# **High-Voltage Switchmode Controller**

## **FEATURES**

- 9- to 80-V Input Range Current-Mode Control
- High Efficiency Operation (> 80%)
- Internal Start-Up Circuit
- High-Speed, Source-Sink Output Drive Internal Oscillator (1 MHz)

# • SHUTDOWN and RESET

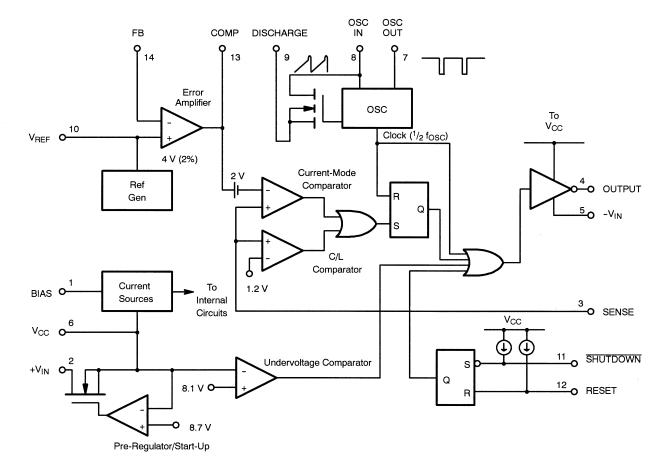
## **DESCRIPTION**

The Si9112 is a BiC/DMOS integrated circuit designed for use in high-efficiency switchmode power converters. A highvoltage DMOS input allows this controller to work over a wide range of input voltages (9- to 80-VDC). Current-mode PWM control circuitry is implemented in CMOS to reduce internal power consumption to less than 10 mW.

A CMOS output driver provides high-speed switching of MOSPOWER devices large enough to supply 50 W of output power. When combined with an output MOSFET and transformer, the Si9112 can be used to implement singleended power converter topologies (i.e., flyback, forward, and cuk).

The Si9112 is available in 14-pin plastic DIP, and SOIC packages, and is specified over the industrial, D suffix (-40 to 85°C) temperature range.

## **FUNCTIONAL BLOCK DIAGRAM**



Application Note AN703 may also be obtained via FaxBack, request document #70577.



# **ABSOLUTE MAXIMUM RATINGS**

Voltages Referenced to $-V_{IN}$ ( $V_{CC} < +V_{IN} + 0.3 \text{ V}$ )	Junction Temperature (T <sub>J</sub> )				
V <sub>CC</sub>	Power Dissipation (Package) <sup>a</sup> 14-Pin Plastic DIP (J Suffix) <sup>b</sup>				
(RËSET, SHUTDOWN, OSC IN)					
HV Pre-Regulator Input Current (continuous)	NOTES  a Device mounted with all leads soldered or welded to PC heard				
Storage Temperature	b. Derate 6 mW/°C above 25°C. c. Derate 7.2 mW/°C above 25°C.				

# **RECOMMENDED OPERATING RANGE**

Voltages Referenced to -V <sub>IN</sub>	$R_{\text{OSC}}$
V <sub>CC</sub>	Linear Inputs
+V <sub>IN</sub>	Digital Inputs
f <sub>OSC</sub>	

SPECIFICATIONS								
Parameter	Symbol	Test Conditions Unless Otherwise Specified	Temp b	<b>Limits</b> D Suffix -40 to 85°C				
		DISCHARGE = $-V_{IN}$ = 0 V $V_{CC}$ = 9 V, $+V_{IN}$ = 12 V $R_{BIAS}$ = 270 k $\Omega$ , $R_{OSC}$ = 330 k $\Omega$		Min <sup>d</sup>	Турс	Max <sup>e</sup>	Unit	
Reference								
Output Voltage	V <sub>R</sub>	OSC IN = - $V_{IN}$ (OSC Disabled) $R_L = 10 \text{ M}\Omega$	Room Full <sup>e</sup>	3.88 3.82	4.0	4.12 4.14	V	
Output Impedance <sup>e</sup>	Z <sub>OUT</sub>		Room	15	30	45	kΩ	
Short Circuit Current	I <sub>SREF</sub>	$V_{REF} = -V_{IN}$	Room	70	100	130	μΑ	
Temperature Stability <sup>e</sup>	T <sub>REF</sub>		Full		0.5	1.0	mV/°C	
Oscillator								
Maximum Frequency <sup>e</sup>	f <sub>MAX</sub>	R <sub>OSC</sub> = 0	Room	1	3		MHz	
Initial Accuracy		R <sub>OSC</sub> = 330 k <sup>f</sup>	Room	80	100	120	l,∐=	
	fosc	R <sub>OSC</sub> = 150 k <sup>f</sup>	Room	160	200	240	kHz	
Voltage Stability	Δf/f	$\Delta f/f = f(13.5 \text{ V}) - f(9.5 \text{ V}) / f(9.5 \text{ V})$	Room		9	15	%	
Temperature Coefficient <sup>e</sup>	Tosc		Full		200	500	ppm/°C	
Error Amplifier								
Feedback Input Voltage	V <sub>FB</sub>	FB Tied to COMP OSC IN = - V <sub>IN</sub> (OSC Disabled)	Room	3.92	4.00	4.08	V	
Input Offset Voltage	Vos	OSC IN = - V <sub>IN</sub> (OSC Disabled)	Room		±15	±40	mV	
Input BIAS Current	I <sub>FB</sub>	OSC IN = - $V_{IN}$ , $V_{FB} = 4 V$	Room		25	500	nA	
Open Loop Voltage Gain <sup>e</sup>	A <sub>VOL</sub>	OSC IN = - V <sub>IN</sub>	Room	60	80		dB	
Unity Gain Bandwidth <sup>e</sup>	BW	OSC IN = - V <sub>IN</sub> (OSC Disabled)	Room	1	1.5		MHz	
Dynamic Output Impedance <sup>e</sup>	Z <sub>OUT</sub>	Error Amp Configured for 60 dB gain	Room		1000	2000	Ω	
Output Current I <sub>O</sub>		Source V <sub>FB</sub> = 3.4 V Room		-2.0	-1.4	mA		
	I <sub>OUT</sub>	Sink V <sub>FB</sub> = 4.5 V	Room	0.12	0.15		] IIIA	
Power Supply Rejection <sup>e</sup>	PSRR	9 V ≤ V <sub>CC</sub> ≤ 13.5 V	Room	50	70		dB	



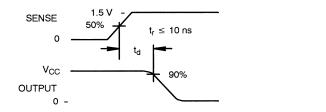
Parameter	Symbol	Test Conditions Unless Otherwise Specified DISCHARGE = -V <sub>IN</sub> = 0 V	<b>Temp</b>	Limits D Suffix -40 to 85°C			
		$V_{CC} = 9 \text{ V}, +V_{IN} = 12 \text{ V}$ $R_{BIAS} = 270 \text{ k}\Omega$ , $R_{OSC} = 330 \text{ k}\Omega$		Min <sup>d</sup>	Тур	Max <sup>e</sup>	Unit
Current Limit							
Threshold Voltage	V <sub>SOURCE</sub>	V <sub>FB</sub> = 0 V	Room	1.1	1.3	1.5	V
Delay to Output <sup>e</sup>	t <sub>d</sub>	V <sub>SENSE</sub> = 1.5 V, See Figure 1.	Room		100	150	ns
Pre-Regulator/Start-Up			-	<u>-</u>		-	
Input Voltage	+V <sub>IN</sub>	I <sub>IN</sub> = 10 μA	Room	80			V
Input Leakage Current	+I <sub>IN</sub>	V <sub>CC</sub> ≥ 9.4 V	Room			10	μΑ
Pre-Regulator Start-Up Current	I <sub>START</sub>	+V <sub>IN</sub> = 48 V	Room	12	20		mA
Pre-Regulator Dropout Voltage	V <sub>CC</sub>	+V <sub>IN</sub> = 10 V, R <sub>LOAD</sub> = 4 k at Pin 6	Room	V <sub>UVLO</sub> +0.1			
V <sub>CC</sub> Pre-Regulator Turn-Off Threshold Voltage	$V_{REG}$	I <sub>PRE-REGULATOR</sub> = 10 μA	Room	8.0	8.7	9.4	V
Undervoltage Lockout	$V_{UVLO}$	See Detailed Description	Room	7.2	8.1	8.9	
V <sub>REG</sub> -V <sub>UVLO</sub>	$V_{DELTA}$		Room	0.3	0.6		
Supply							
Supply Current	I <sub>CC</sub>	C <sub>L</sub> ≤ 75 pF (Pin 4)	Room		0.6	1.0	mA
Bias Current	I <sub>BIAS</sub>		Room		15		μΑ
Logic							
SHUTDOWN Delay <sup>e</sup>	t <sub>SD</sub>	$C_L = 500 \text{ pF}$ $V_{SENSE} = -V_{IN}$ , See Figure 2.	Room		50	100	
SHUTDOWN Pulse Width <sup>e</sup>	t <sub>SW</sub>		Room	50			ns
RESET Pulse Width <sup>e</sup>	$t_{RW}$	See Figure 3.	Room	50			113
Latching Pulse Width SHUTDOWN and RESET Low <sup>e</sup>	t <sub>LW</sub>	Ü	Room	25			
Input Low Voltage	$V_{IL}$		Room			2.0	V
Input High Voltage	$V_{IH}$		Room	7.0			v
Input Current Input Voltage High	I <sub>IH</sub>	V <sub>LOGIC</sub> = V <sub>CC</sub>	Room		1	5	μΑ
Input Current Input Voltage Low	I <sub>IL</sub>	V <sub>IN</sub> = 0 V	Room	-35	25		
Output							
Output High Voltage	V <sub>OH</sub>	I <sub>OUT</sub> = -10 mA	Room Full	8.7 8.5			V
Output Low Voltage	V <sub>OL</sub>	I <sub>OUT</sub> = 10 mA	Room Full			0.3 0.5	v
Output Resistance <sup>e</sup>	R <sub>OUT</sub>	I <sub>OUT</sub> = 10 mA, Source or Sink	Room Full		20 25	30 50	Ω
Rise Time <sup>e</sup>	t <sub>r</sub>	C <sub>L</sub> = 500 pF	Room		40	75	ns
Fall Time <sup>e</sup>	t <sub>f</sub>	ο <sub>L</sub> = 500 βι	Room		40	75	113

#### Notes

- a. Refer to PROCESS OPTION FLOWCHART for additional information.
- b. Room =  $25^{\circ}$ C, Full = as determined by the operating temperature suffix.
- c. Typical values are for DESIGN AID ONLY, not guaranteed nor subject to production testing.
- d. The algebraic convention whereby the most negative value is a minimum and the most positive a maximum.
- e. Guaranteed by design, not subject to production test.
- f.  $C_{STRAY}$  Pin 8 =  $\leq$  5 pF.

# VISHAY

# **TIMING WAVEFORMS**



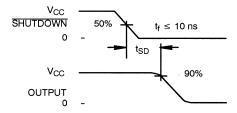


FIGURE 1.

FIGURE 2.

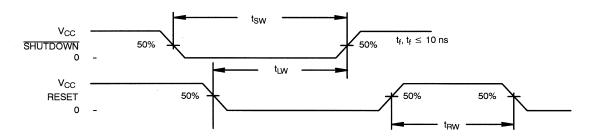
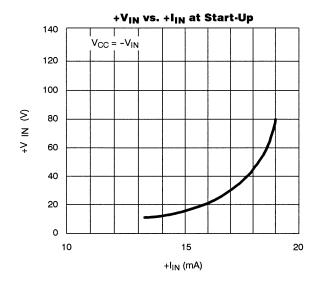


FIGURE 3.

# **TYPICAL CHARACTERISTICS**



Output Switching Frequency vs. Oscillator Resistance

1 M

10 k

10 k

10 k

10 k

10 c

1 M

10 c

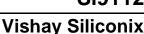
1 M

1 M

1 M

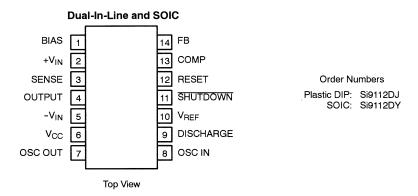
1 M

FIGURE 4. FIGURE 5.





#### PIN CONFIGURATIONS



## **DETAILED DESCRIPTION**

## Pre-Regulator/Start-Up Section

Due to the low quiescent current requirement of the Si9112 control circuitry, bias power can be supplied from the unregulated input power source, from an external regulated low-voltage supply, or from an auxiliary "bootstrap" winding on the output inductor or transformer.

When power is first applied during start-up, +V $_{\rm IN}$  (pin 2) will draw a constant current. The magnitude of this current is determined by a high-voltage depletion MOSFET device which is connected between +V $_{\rm IN}$  and V $_{\rm CC}$  (pin 6). This start-up circuitry provides initial power to the IC by charging an external bypass capacitance connected to the V $_{\rm CC}$  pin. The charging current is disabled when V $_{\rm CC}$  exceeds 8.7 V. If V $_{\rm CC}$  is not forced to exceed the 8.7-V threshold, then V $_{\rm CC}$  will be regulated to a nominal value of 8.7 V by the pre-regulator circuit.

As the supply voltage rises toward the normal operating conditions, an internal undervoltage (UV) lockout circuit keeps the output driver disabled until  $V_{CC}$  exceeds the UV lockout threshold (typically 8.1 V). This guarantees that the control logic will be functioning properly and that sufficient gate drive voltage is available before the MOSFET turns on. The design of the IC is such that the undervoltage lockout threshold will be at least 300 mV less than the pre-regulator turn-off voltage. Power dissipation can be minimized by providing an external power source to  $V_{CC}$  such that the pre-regulator circuit is disabled.

# **BIAS**

To properly set the bias for the Si9112, a 270-k $\Omega$  resistor should be tied from BIAS (pin 1) to -V<sub>IN</sub> (pin 5). This

determines the magnitude of bias current in all of the analog sections and the pull-up current for the  $\overline{SHUTDOWN}$  and RESET pins. The current flowing in the bias resistor is nominally 15  $\mu$ A.

#### **Reference Section**

The reference section of the Si9112 consists of a temperature compensated buried zener and trimmable divider network. The output of the reference section is connected internally to the non-inverting input of the error amplifier. Nominal reference output voltage is 4 V. The trimming procedure that is used on the Si9112 brings the output of the error amplifier (which is configured for unity gain during trimming) to within ±2% of 4 V. This automatically compensates for input offset voltage in the error amplifier.

The output impedance of the reference section has been purposely made high so that a low impedance external voltage source can be used to override the internal voltage source, if desired, without otherwise altering the performance of the device.

## **Error Amplifier**

Closed-loop regulation is provided by the error amplifier. The emitter follower output has a typical dynamic output impedance of 1000  $\Omega,$  and is intended for use with "around-the-amplifier" compensation. A MOS differential input stage provides low input leakage current. The noninverting input to the error amplifier (V $_{\rm REF}$ ) is internally connected to the output of the reference supply and should be bypassed with a small capacitor to ground.



#### **Oscillator Section**

The oscillator consists of a ring of CMOS inverters, capacitors, and a capacitor discharge switch. Frequency is set by an external resistor between the OSC IN and OSC OUT pins. (See Typical Characteristics for details of resistor value vs. frequency.) The DISCHARGE pin should be tied to -V<sub>IN</sub> for normal internal oscillator operation. A frequency divider in the logic section limits switch duty cycle to  $\leq\!50\%$  by locking the switching frequency to one half of the oscillator frequency.

Remote synchronization can be accomplished by capacitive coupling of a SYNC pulse into the OSC IN (pin 8) terminal. For a 5-V pulse amplitude and 0.5- $\mu$ s pulse width, typical values would be 100 pF in series with 3 k $\Omega$  to pin 8.

## **SHUTDOWN** and RESET

SHUTDOWN (pin 11) and RESET (pin 12) are intended for overriding the output MOSFET switch via external control logic. The two inputs are fed through a latch preceding the output switch. Depending on the logic state of RESET, SHUTDOWN can be either a latched or unlatched input. The output is off whenever SHUTDOWN is low. By simultaneously having SHUTDOWN and RESET low, the latch is set and SHUTDOWN has no effect until RESET goes high. The truth table for these inputs is given in Table 1.

TABLE 1. Truth Table for the SHUTDOWN and RESET Pins

SHUTDOWN	RESET	Output
Н	Н	Normal Operation
Н	TŁ.	Normal Operation (No Change)
L	Н	Off (Not Latched)
L	L	Off (Latched)
F	L	Off (Latched, No Change)

Both pins have internal current source pull-ups and should be left disconnected when not in use. An added feature of the current sources is the ability to connect a capacitor and an open-collector driver to the SHUTDOWN or RESET pins to provide variable shutdown time.

## **Output Driver**

The push-pull driver output has a typical on-resistance of  $20~\Omega$ . Maximum switching times are specified at 75 ns for a 500 pF load. This is sufficient to directly drive 60-V, 25-A MOSFETs. Larger devices can be driven, but switching times will be longer, resulting in higher switching losses.

For applications information refer to AN703.